

Exam CT4150 Plasticity Theory
Thursday 18 January 2007, 9:00 – 12:00 hours

Problem 1

A frame consists of members with a strength $5M_p$ and a column with a strength M_p (Fig. 1). The frame has pin connections with the foundation. The frame is loaded by four forces. The following relation exists between the plastic moment M_p and the plastic normal force N_p (Fig. 2).

$$N_p = \beta \frac{M_p}{a}$$

The influence of shear on the yield contour is neglected. Buckling and second order effects are not considered.

- a** Assume $\beta \rightarrow \infty$. Determine the collapse load F for each possible mechanism. Write the collapse loads as functions of M_p and a . What is the decisive collapse load? (1.5 points)

- b** Assume $\beta \rightarrow \infty$. Draw the bending moment diagram of the structure at the moment of collapse. (1 point)

- c** Assume $\beta = 43\sqrt{2}$. Choose one of the following problems (You need not do both).
- Determine the largest lower-bound for F .
 - Determine the smallest upper-bound for F .

For the upper-bound you only need to write down the equations and not to solve them. Use the decisive mechanism of problem **1a**. (2 points)

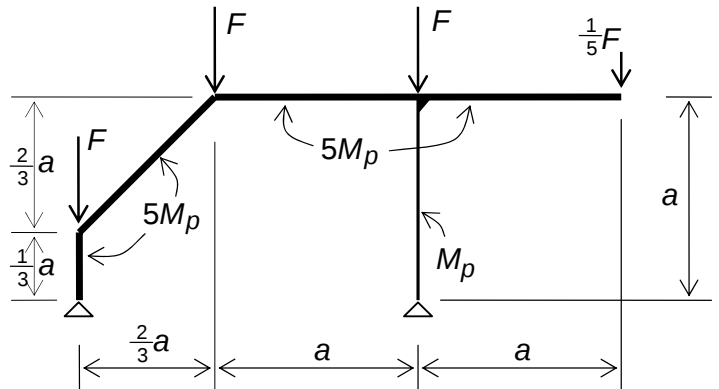


Figure 1. Frame

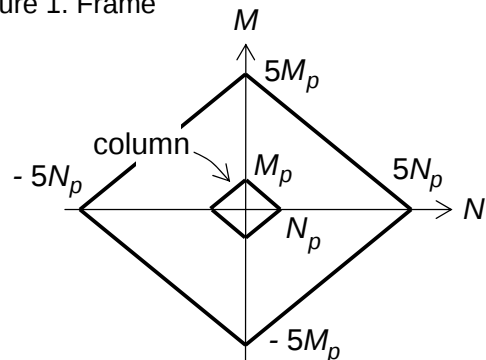


Figure 2. Yield contours of the frame members

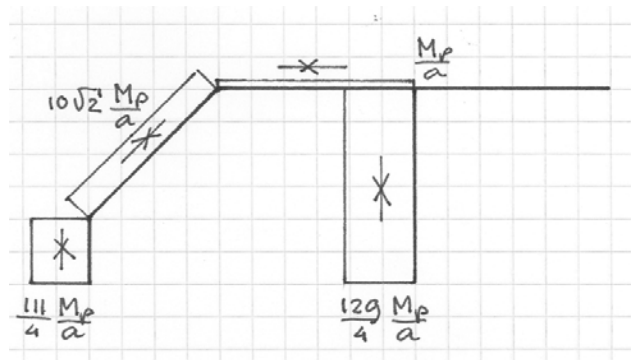


Figure 3. Normal force diagram of the frame

Problem 2

A plate is fixed at eight edges and free at four edges (Figure 3). The plate carries an evenly distributed load q [kN/m²]. The plate is homogeneous.

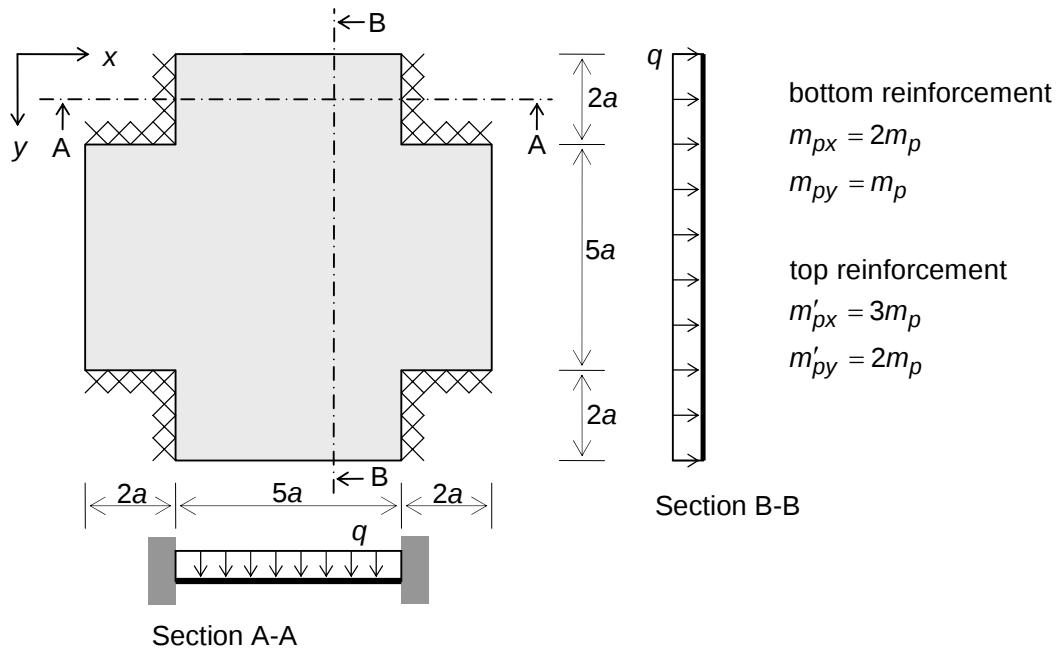


Figure 4. Plate with fixed and free edges

- a We consider the yield line patterns of Figure 5. Which of these patterns give kinematically possible mechanisms. (1 point)

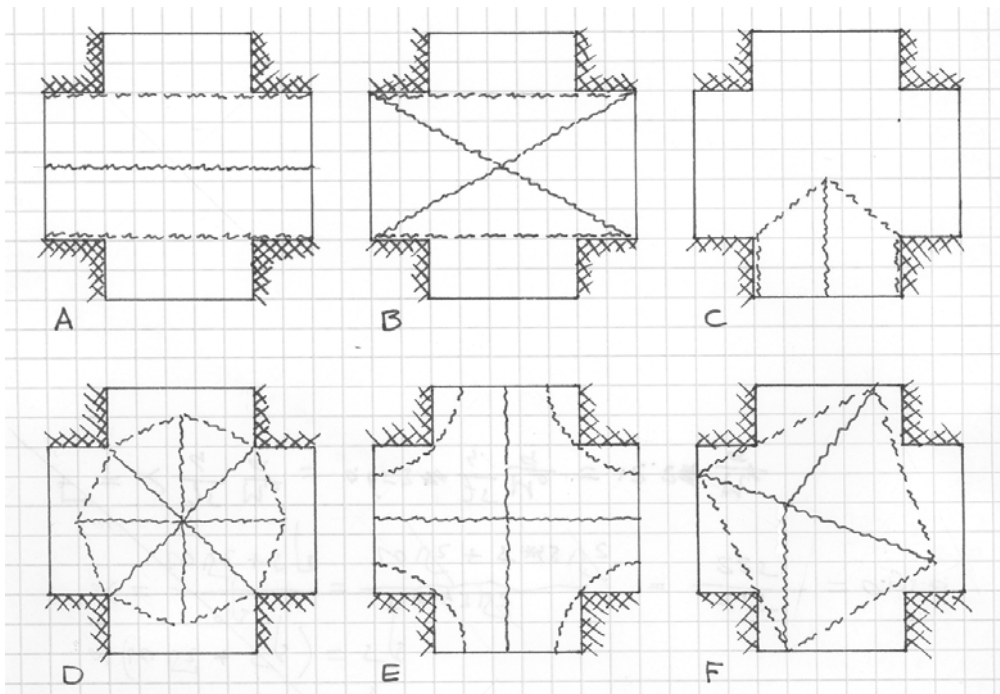


Figure 5. Yield line patterns of problem 2a

- b We consider the yield line pattern of Figure 6. Determine an upper bound for q expressed in m_p and a . (1.5 points)

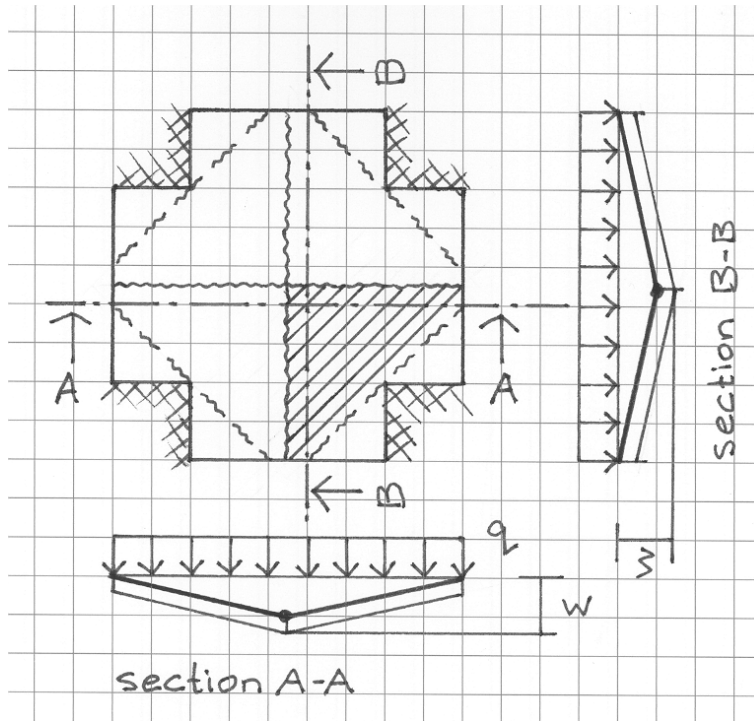


Figure 6. Yield line pattern of problem 2b

- c Determine the largest lower-bound for q using torsion free beams ($m_{xy} = 0$) in the x direction and y direction. (1.5 points)

Problem 3

- a Consider a small plate part with only a torsion moment $m_{xy} > 0$ (Fig. 7). The reinforcement is in the directions x and y . What is the direction of a positive yield line when $m_{px} > m_{py}$? Choose A, B or C. (0.5 points)

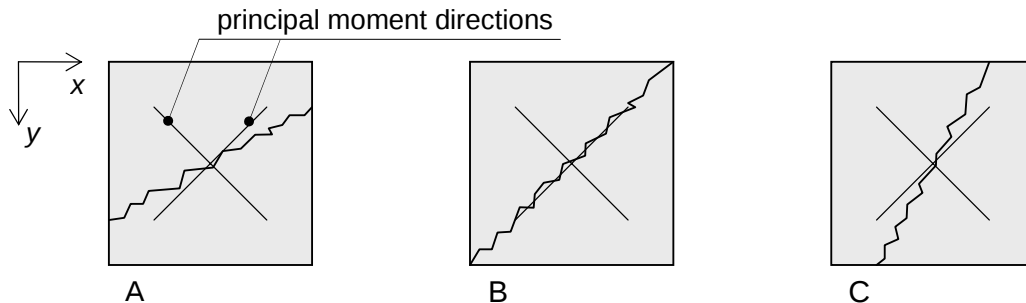


Figure 7. Plate parts with yield lines

- b No homogenous isotropic plate can carry a point load larger than $F = 4\pi m_p$. Explain this. (1 point)

Answer to Problem 1a 18 January 2007

$$E = 5M_p(6\theta + \frac{3}{2}\theta) + 5M_p(\frac{3}{2}\theta + \theta)$$

$$= 50M_p\theta$$

$$A = Fa\theta - \frac{1}{5}Fa\theta = \frac{4}{5}aF\theta$$

$$E = A \Rightarrow F = \frac{125}{2} \frac{M_p}{a}$$

$$E = 5M_p\theta$$

$$A = \frac{1}{5}Fa\theta$$

$$E = A \Rightarrow F = 25 \frac{M_p}{a}$$

$$E = M_p\theta + 5M_p3\theta$$

$$A = F \times 0$$

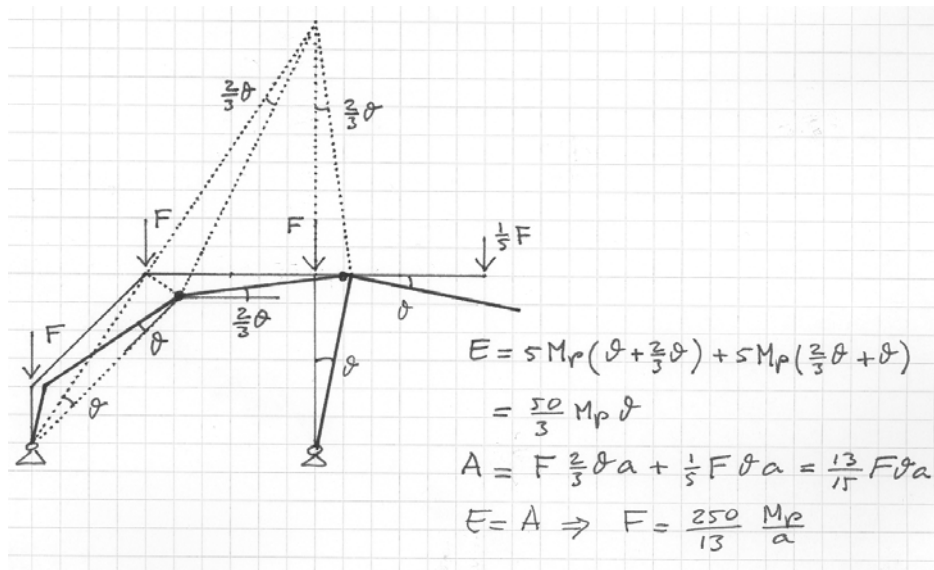
$$E = A \Rightarrow F = \infty$$

$$E = 5M_p(\theta + \frac{2}{3}\theta) + M_p(\frac{2}{3}\theta + \theta)$$

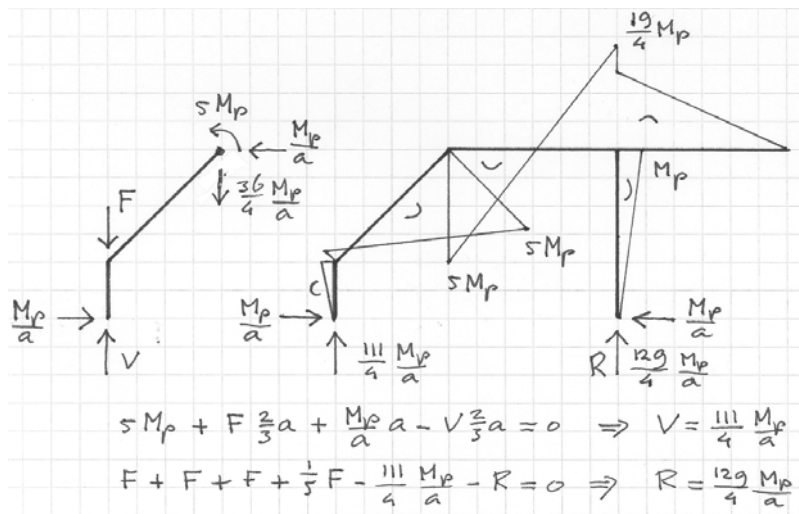
$$= 10M_p\theta$$

$$A = F\frac{2}{3}\theta a - \frac{1}{5}F\frac{2}{3}\theta a = \frac{8}{15}F\theta a$$

$$\boxed{F = \frac{75}{4} \frac{M_p}{a}} \leftarrow \text{decisive}$$



Answer to Problem 1b



Answer to problem 1c Lower-bound

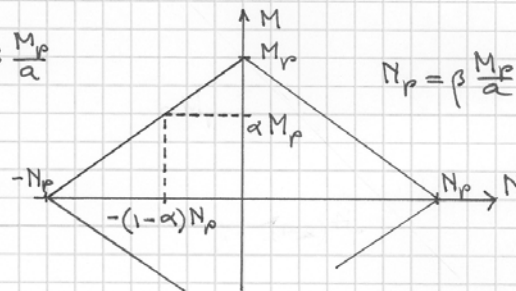
We reduce the loading, moments and normal forces such that everywhere the yield condition is fulfilled. In the column head with a moment αM_p we can allow a force $(1-\alpha)N_p$.

$$N = \alpha \frac{129}{4} \frac{M_p}{a} = (1-\alpha)N_p = (1-\alpha)\beta \frac{M_p}{a}$$

$$\alpha \frac{129}{4} = (1-\alpha)\beta$$

$$\alpha \left(\frac{129}{4} + \beta \right) = \beta$$

$$\alpha = \frac{\beta}{\frac{129}{4} + \beta} = \frac{43\sqrt{2}}{\frac{129}{4} + 43\sqrt{2}} = 0,653$$



In the inclined beam with a moment $\alpha 5 M_p$ we can allow a force $(1-\alpha) 5 N_p$

$$N = \alpha 10\sqrt{2} \frac{M_p}{a} = (1-\alpha) 5 N_p = (1-\alpha) 5 \beta \frac{M_p}{a}$$

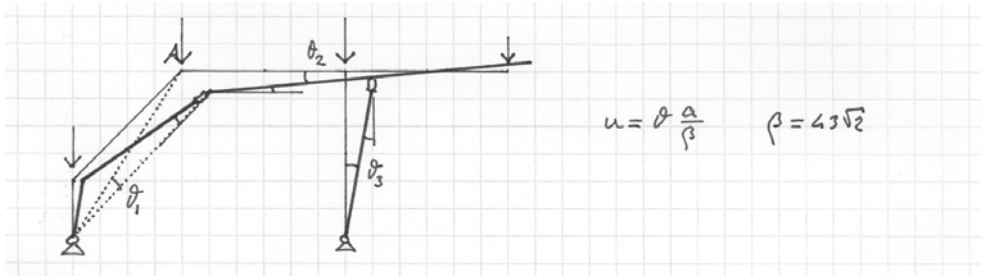
$$\alpha 10\sqrt{2} = (1-\alpha) 5 \beta$$

$$\alpha (10\sqrt{2} + 5\beta) = 5\beta$$

$$\alpha = \frac{5\beta}{10\sqrt{2} + 5\beta} = \frac{5 \times 43\sqrt{2}}{10\sqrt{2} + 5 \times 43\sqrt{2}} = \frac{215}{225} = 0,956$$

$$F = \alpha \frac{75}{4} \frac{M_p}{a} = 0,653 \frac{75}{4} \frac{M_p}{a} = 12,2 \frac{M_p}{a}$$

Answer to Problem 1c Upper-bound



horizontal displacement of A $\rightarrow$

$$\theta_1 a - (\theta_1 + \theta_2) \frac{a}{\beta} \frac{1}{\sqrt{2}} = \theta_3 a$$

vertical displacement of A $\downarrow$

$$\theta_1 \frac{2}{3} a + (\theta_1 + \theta_2) \frac{a}{\beta} \frac{1}{\sqrt{2}} = (\theta_2 + \theta_3) \frac{a}{\beta} + \theta_2 a$$

$$A = F \left[\theta_1 \frac{2}{3} a + (\theta_1 + \theta_2) \frac{a}{\beta} \frac{1}{\sqrt{2}} \right] + F (\theta_2 + \theta_3) \frac{a}{\beta} - \frac{1}{5} F \left[\theta_2 a - (\theta_2 + \theta_3) \frac{a}{\beta} \right]$$

$$E = 5 M_p (\theta_1 + \theta_2) + M_p (\theta_2 + \theta_3)$$

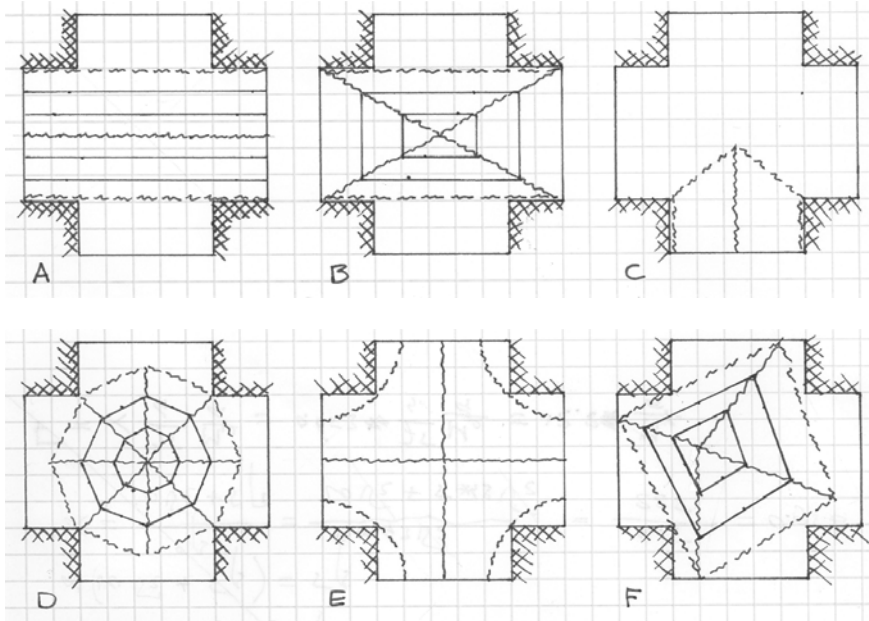
$$A = E$$

the solution is computed by Maple

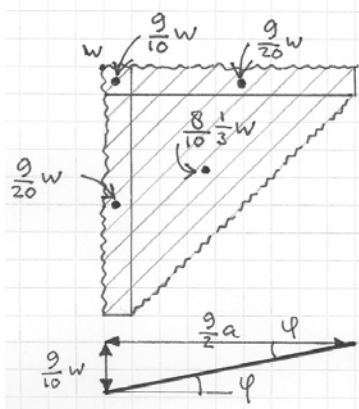
$$\theta_1 = 1,52 \theta_2 \quad \theta_3 = 1,49 \theta_2 \quad F = 16,9 \frac{M_p}{a}$$

Answer to Problem 2a

Kinematically possible are patterns A, B, D and F. The figure below shows the altitude lines of the deformed mechanisms.



Answer to Problem 2b



$$A = 4 \left[q \frac{(4a)^2}{2} \frac{8}{30} w + 2 \left(q 4a \frac{1}{2} a \frac{9}{20} w \right) + q \left(\frac{a}{2} \right)^2 \frac{9}{10} w \right]$$

$$= \frac{499}{30} q a^2 w$$

$$\varphi = \frac{\frac{9}{20} w}{\frac{9}{2} a} = \frac{1}{5} \frac{w}{a}$$

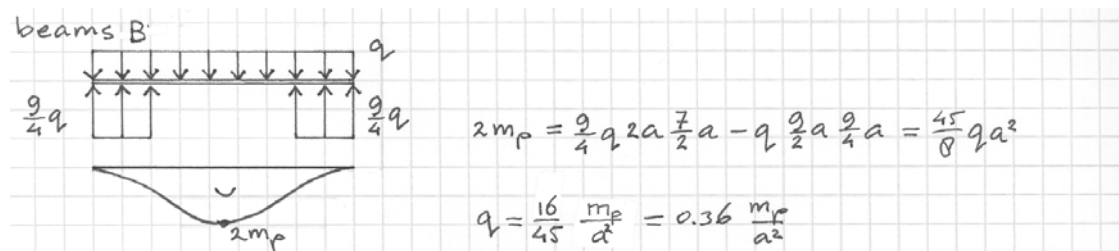
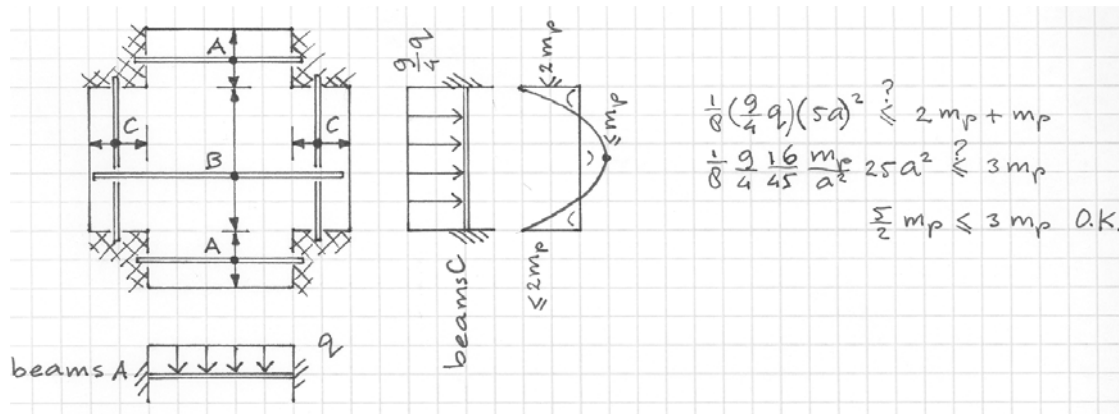
$$E = 2 m_p 2 \frac{1}{5} \frac{w}{a} g a + m_p 2 \frac{1}{5} \frac{w}{a} g a +$$

$$+ 4 \left[3 m_p \frac{1}{5} \frac{w}{a} 4a + 2 m_p \frac{1}{5} \frac{w}{a} 4a \right]$$

$$= \frac{134}{5} m_p w$$

$$A = E \Rightarrow q = \frac{804}{499} \frac{m_p}{a^2} = 1,61 \frac{m_p}{a^2}$$

Answer to Problem 2c



Answer to Problem 3a

A: The yield line will try crossing mainly weaker reinforcing bars (Lecture book p. 64)

Answer to Problem 3b

$4\pi m_p$ is the collapse load of a circular plate fixed on the edge. This circular yield line pattern (Lecture book Fig. 10.2) is possible in any plate for a point load somewhere on its interior. If the point load acts on an edge the upper-bound is smaller (Lecture book Fig. 10.4). Therefore, $4\pi m_p$ is a general upper-bound.