

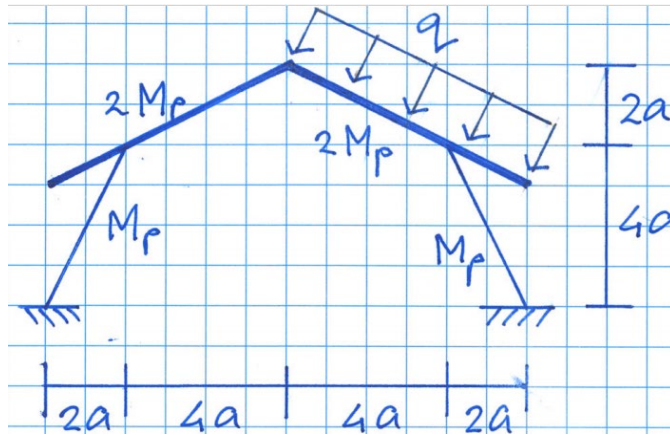


Figure 1. Frame structure

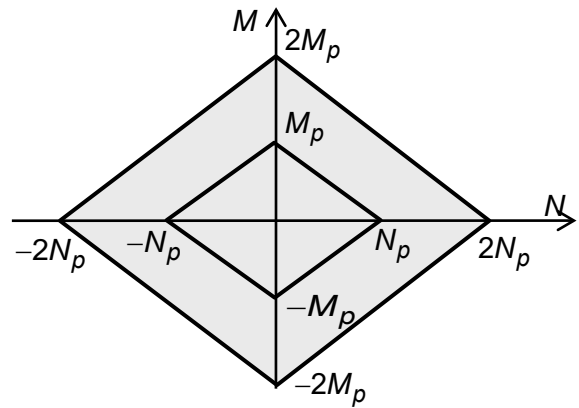


Figure 2. Yield contours

Problem 1

A frame consists of four members (Fig.1). The columns have a strength M_p . The roof members have a strength $2M_p$. All members are rigidly connected. The supports are fixed. The structure is loaded by an evenly distributed line load q per length of roof member (wind load). The relation of Figure 2 exists between the plastic moments and the plastic normal forces.

$$N_p = \beta \frac{M_p}{a}$$

The influence of shear on the yield contour is neglected. Buckling and second order effects are not considered.

- a** Assume $\beta \rightarrow \infty$. Determine the collapse load q for all possible mechanisms. Write the collapse loads as functions of M_p and a . What is the decisive collapse load? (1.5 point)
- b** Assume $\beta \rightarrow \infty$. Draw the bending moment diagram and normal force diagram for the structure at the moment of collapse. (1.5 points)
- c** Assume $\beta = 7$. Choose one of the following problems (You need not do both).
 - Determine the largest lower-bound for q .
 - Determine the smallest upper-bound for q .
You only need to write down the equations and not solve the equations (1.5 points).

Problem 2

A reinforced concrete plate has simply supported edges and free edges (Fig. 3). It carries an evenly distributed load p [kN/m²]. There is no other load on the plate. The plate is homogeneous and orthotropic.

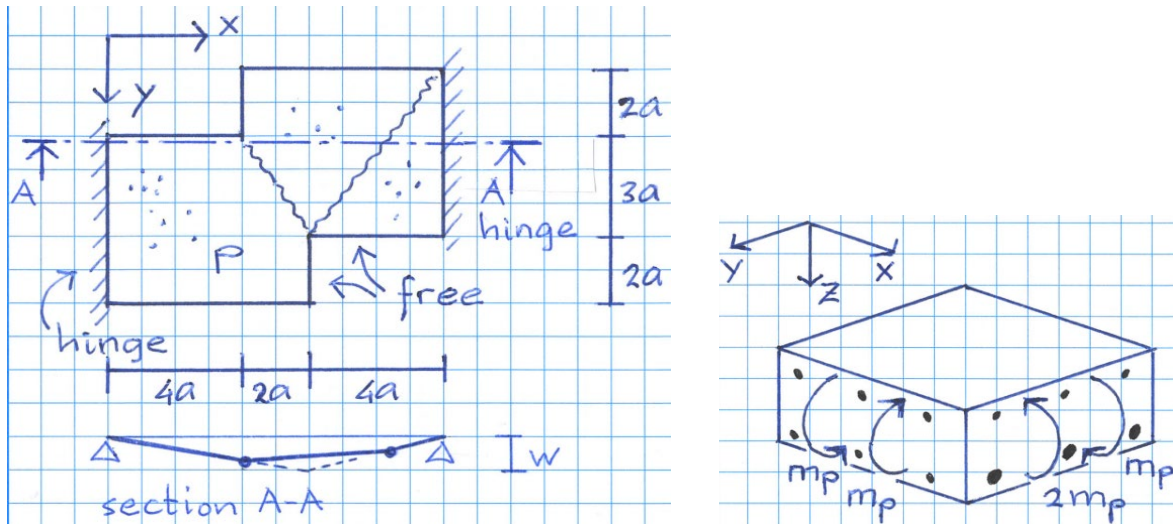


Figure 3. Plate dimensions and reinforcement

- a Consider the yield line patterns of Figure 4. Which of these patterns give kinematically possible mechanisms? (1 point)

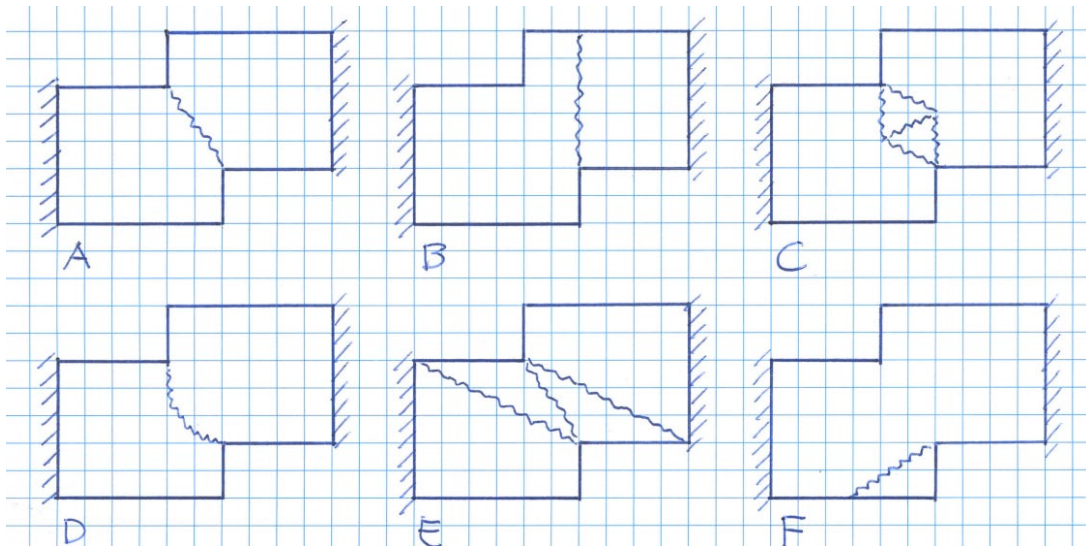


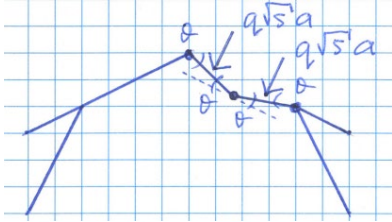
Figure 4. Yield line patterns of problem 2a

- b Consider the yield line pattern of Figure 3. Determine an upper bound for p expressed in m_p and a (1.5 point).
- c Determine the largest lower-bound for p using torsion free beams ($m_{xy} = 0$). You only need to write down the equations and not solve the equations. (1.5 point)

Problem 3

- a** Which yield criterion is used for stainless steel? (0.5 point)
- b** What is normality of the plastic deformation? (0.5 point)
- c** What is the relation between mechanism and statically indetermined? (0.5 point)

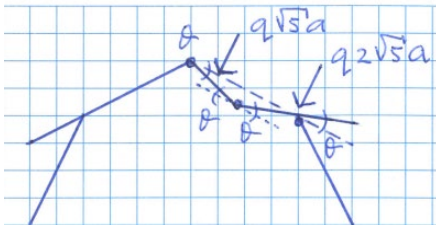
Answer to problem 1a



$$E = 2M_p\theta + 2M_p(\theta + \theta) + 2M_p\theta$$

$$A = 2(q\sqrt{5}a\theta \frac{\sqrt{5}}{2}a)$$

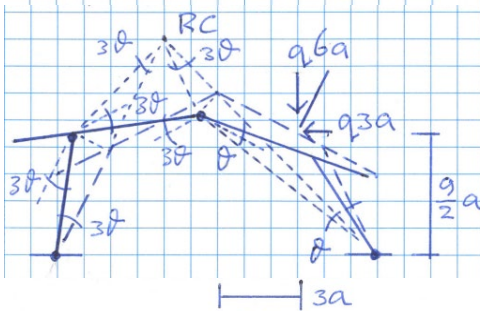
$$E = A \Rightarrow q = \frac{8}{5} \frac{M_p}{a^2}$$



$$E = 2M_p\theta + 2M_p(\theta + \theta) + M_p\theta$$

$$A = q\sqrt{5}a\theta \frac{\sqrt{5}}{2}a$$

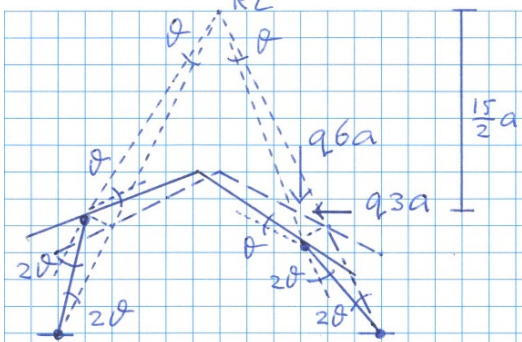
$$E = A \Rightarrow q = \frac{14}{5} \frac{M_p}{a^2}$$



$$E = M_p3\theta + M_p(3\theta + 3\theta) + 2M_p(3\theta + \theta) + M_p\theta$$

$$A = q3a\theta \frac{9}{2}a + q6a\theta 3a$$

$$E = A \Rightarrow q = \frac{4}{7} \frac{M_p}{a^2}$$

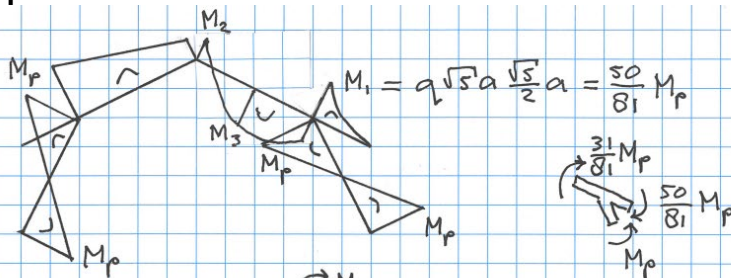


$$E = M_p2\theta + M_p(2\theta + \theta) + M_p(\theta + 2\theta) + M_p2\theta$$

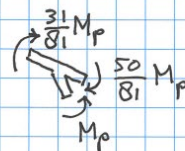
$$A = q3a\theta \frac{15}{2}a + q6a\theta 3a$$

$$E = A \Rightarrow q = \frac{20}{81} \frac{M_p}{a^2} \quad \text{decisive}$$

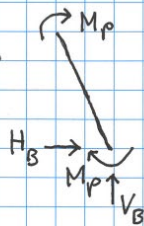
Answer to problem 1b



$$M_1 = q\sqrt{5}a \frac{\sqrt{5}}{2}a = \frac{50}{81} M_p$$



$$\textcircled{1} M_p = H_B 4a + V_B 2a - M_p$$



$$\textcircled{2} \quad M_p = V_B 12a - q_6 a g a + q_3 a \frac{9}{2} a - M_p$$

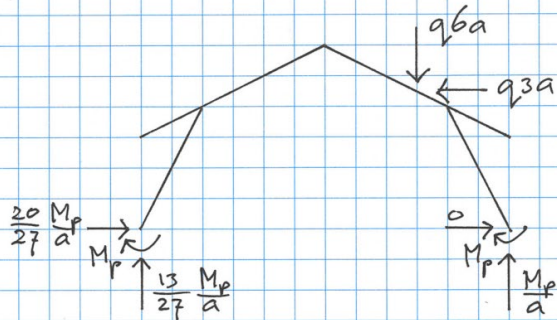
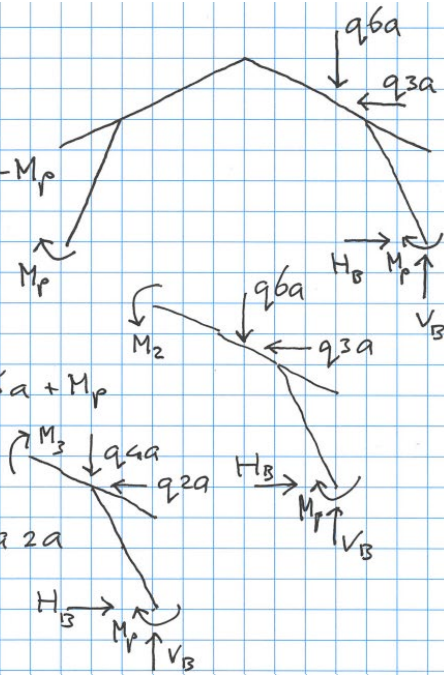
$$\textcircled{1} \quad \left. \begin{array}{l} H_B = 0 \\ V_B = \frac{M_p}{a} \end{array} \right\}$$

$$M_2 = q_6 a 3a + q_3 a \frac{3}{2} a - H_B 6a - V_B 6a + M_p$$

$$= \frac{5}{9} M_p$$

$$M_3 = V_B 4a + H_B 5a - M_p - q_2 a a - q_4 a 2a$$

$$= \frac{43}{81} M_p$$

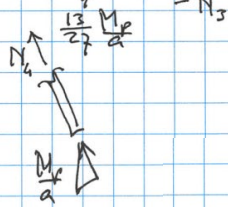


$$N_1 = \left(-\frac{13}{27} \frac{M_p}{a} \frac{2}{\sqrt{5}} + \frac{20}{27} \frac{M_p}{a} \frac{1}{\sqrt{5}} \right) = -0,76 \frac{M_p}{a}$$

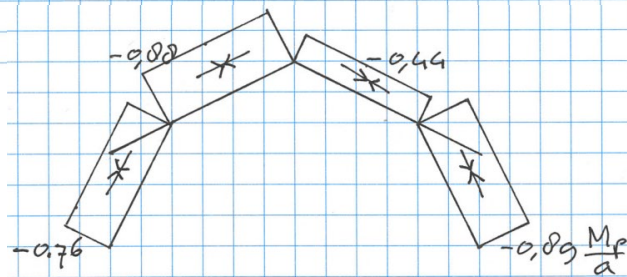
$$q_6 a - \frac{M_p}{a} = \frac{13}{27} \frac{M_p}{a}$$

$$N_2 = - \left(q_3 a \frac{2}{\sqrt{5}} + \frac{13}{27} \frac{M_p}{a} \frac{1}{\sqrt{5}} \right) = -0,88 \frac{M_p}{a}$$

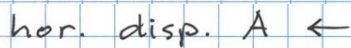
$$N_3 = - \left(q_3 a \frac{2}{\sqrt{5}} + \frac{13}{27} \frac{M_p}{a} \frac{1}{\sqrt{5}} \right) = -0,44 \frac{M_p}{a}$$



$$N_4 = - \frac{M_p}{a} \frac{2}{\sqrt{5}} = -0,89 \frac{M_p}{a}$$



Upperbound



vert. disp. $A \downarrow$

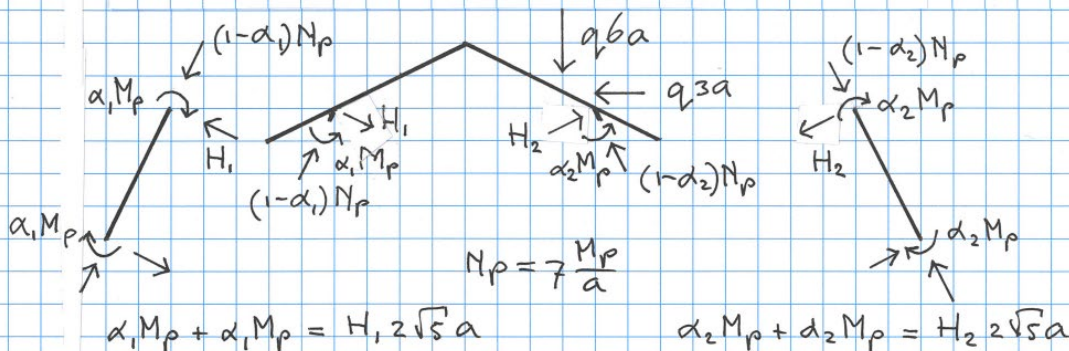
$$E = M_p \vartheta_1 + M_p(\vartheta_1 + \vartheta_2) + M_p(\vartheta_2 + \vartheta_3) + M_p \vartheta_3$$

$$E = A$$

$$q = 0,2207 \frac{M_p}{a^2} \quad \theta_1 = 1,91 \theta_2 \quad \theta_3 = 2,07 \theta_2$$
$$q_{6a} = (1 - \alpha_1) N_p \frac{2}{\sqrt{5}} - H_1 \frac{1}{\sqrt{5}} + (1 - \alpha_2) N_p \frac{2}{\sqrt{5}} + H_2 \frac{1}{\sqrt{5}}$$

$$q_{3a} = (1-\alpha_1)N_p \frac{1}{\sqrt{5}} + H_1 \frac{2}{\sqrt{5}} - (1-\alpha_2)N_p \frac{1}{\sqrt{5}} + H_2 \frac{2}{\sqrt{5}}$$

$$\alpha_1 M_p = q_6 a_7 a - q_3 a \frac{a}{2} - \alpha_2 M_p - (1 - \alpha_2) N_p \frac{2}{\sqrt{5}} \delta a - H_2 \frac{1}{\sqrt{5}} \delta a$$


$$q_v = 0,2207 \frac{\text{Mp}}{\text{a}^2} \quad \alpha_1 = 0,90 \quad \alpha_2 = 0,89 \quad H_1 = 0,40 \frac{\text{Mp}}{\text{a}} \quad H_2 = 0,40 \frac{\text{Mp}}{\text{a}}$$

Answer to problem 2a

B, E, F

(E can move in two ways; so it has too many yield lines)

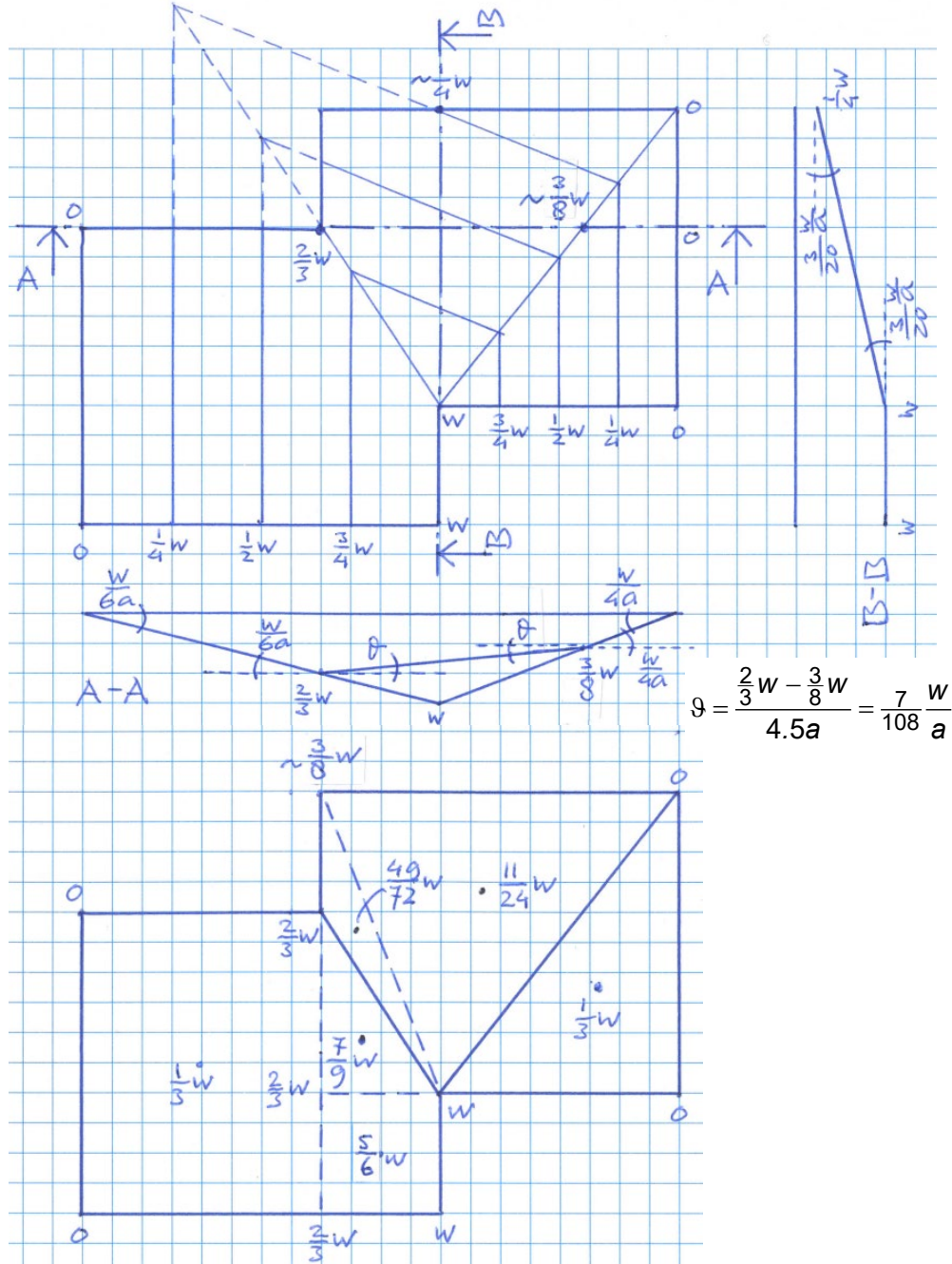
3 or less correct 0.0 point

4 correct 0.3 point

5 correct 0.7 point

6 correct 1.0 point

Answer to problem 2b



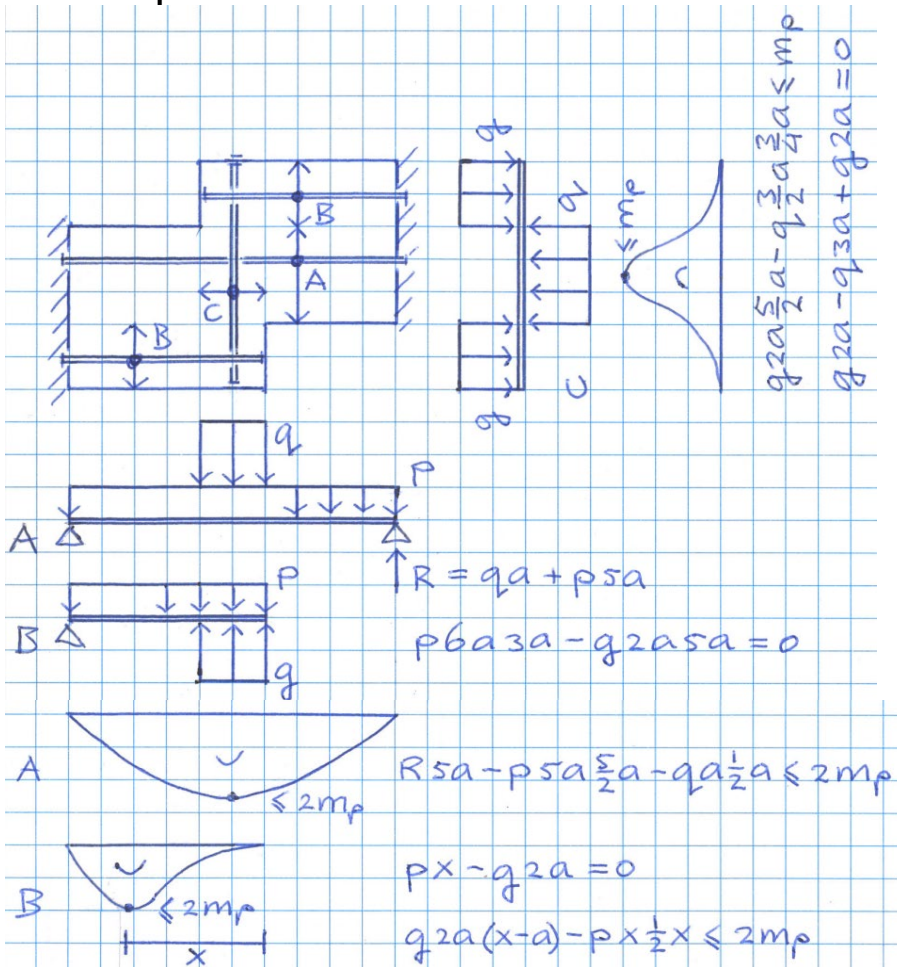
$$E = 2m_p 3a \left(\frac{w}{6a} + \frac{7w}{108a} \right) + m_p 2a \frac{3}{20} \frac{w}{a} + 2m_p 5a \left(\frac{w}{4a} - \frac{7w}{108a} \right) + m_p 4a \frac{3}{20} \frac{w}{a}$$

$$A = p 4a 5a \frac{1}{3} w + p 2a 2a \frac{5}{6} w + p \frac{2a 3a}{2} \frac{7}{9} w + p \frac{4a 5a}{2} \frac{1}{3} w +$$

$$+ p \frac{6a 5a}{2} \frac{11}{24} w + p \frac{2a 2a}{2} \frac{49}{72} w$$

$$E = A \Rightarrow p = 0,173 \frac{m_p}{a^2}$$

Answer to problem 2c



```
> eq1:= R=q*a+p*5*a:
> eq2:= p*6*a*3*a-q*2*a*5*a=0:
> eq3:= R*5*a-p*5*a*5/2*a-q*a*1/2*a=2*mp:
> eq4:= p*x-q*2*a=0:
> eq5:= g*2*a*(x-a)-p*x*1/2*x<2*mp:
> eq6:= g*2*a*5/2*a-q*3/2*a*3/4*a<mp:
> eq7:= g*2*a-q*3*a+g*2*a=0:
> opl:=solve({eq1,eq2,eq3,eq4,eq7},{R,x,p,g,q}); assign(opl):
```

$$opl := \left\{ R = \frac{148 \text{ } mp}{233 \text{ } a}, g = \frac{36 \text{ } mp}{233 \text{ } a^2}, p = \frac{20 \text{ } mp}{233 \text{ } a^2}, q = \frac{48 \text{ } mp}{233 \text{ } a^2}, x = \frac{18 \text{ } a}{5} \right\}$$

> evalf(eq5) ;

$$0.2472103004 \text{ } mp < 2. \text{ } mp$$

> evalf(eq6) ;

$$0.5407725322 \text{ } mp < mp$$

Answer to problem 3

- a Von Mises
- b The vector perpendicular to the yield surface gives the plastic deformations.
- c The number of plastic hinges required for a *mechanism* is less than or equal to the degree of *statically indeterminacy* plus one.

